

# Diagenetic reactions during deep burial in sedimentary basins. Consequences for differential stresses.

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FORCE Meeting NPD. 10. November 2010

# What is HPHT Reservoirs?

**Temperature > 140-150 C ?**

**Fluid pressure > 50 MPa ?**

**With over pressure? 100 MPa ?**

**Requirements :**

Preservation of porosity at great depth due to retarded quartz cementation( clay coatings micro quartz etc).

**Cap rock integrity :** Slightly permeable cap rock or lateral drainage.

In most cases the quality of sandstone reservoirs reaches critical values at about 4 Km depth (130 °C)

**HPHT are exceptions to the rules of normal diagenesis.**

**There is a reason why there is still sufficient porosity at great depth and why there is still oil or gas in the reservoir.**

The diagenetic processes are the same in all basins, but the sediment compositions and the temperature history vary greatly.

# Haltenbanken - Effect of lateral drainage

*V. Storvoll et al. / Marine and Petroleum Geology 19 (2002) 767-781*

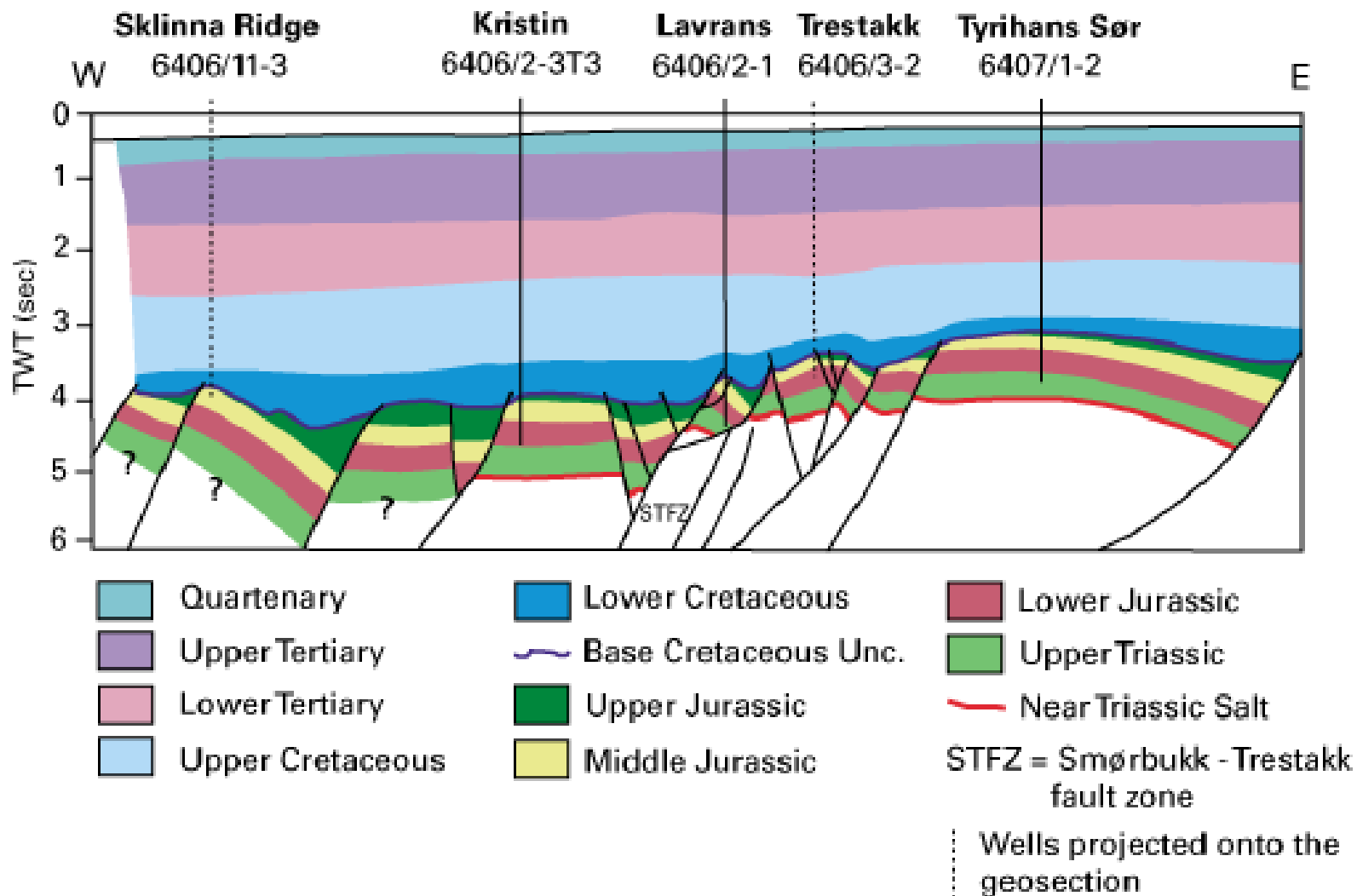
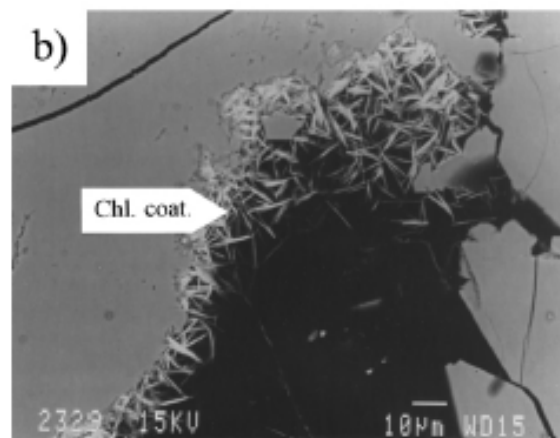
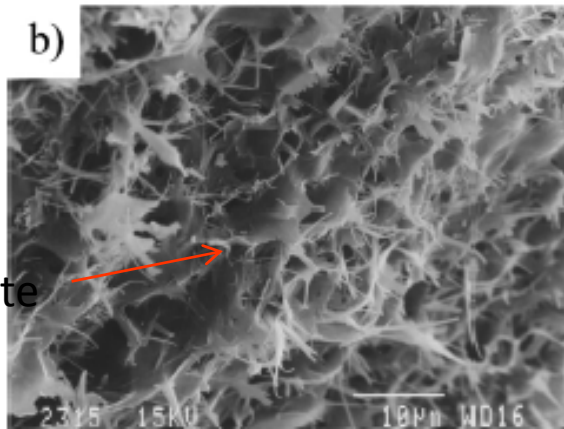
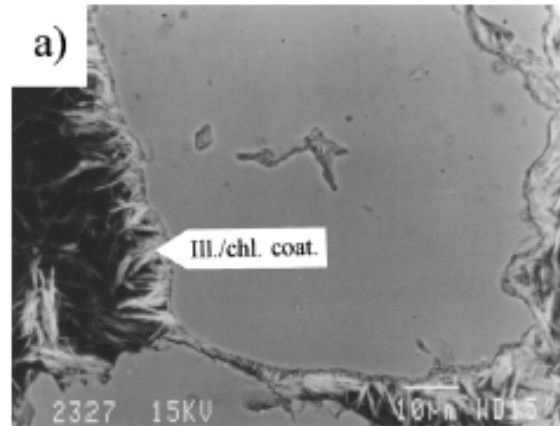
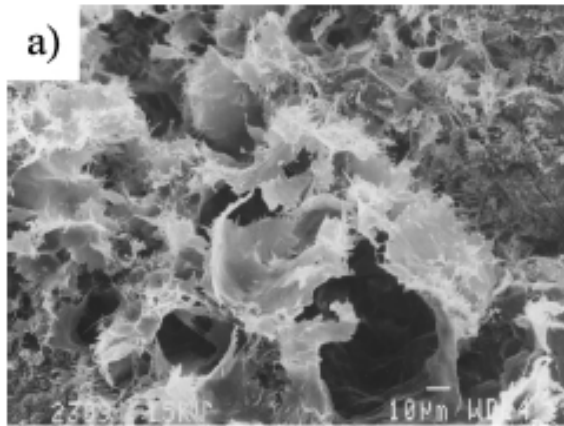


Fig. 3. Cross-section through the Haltenbanken area. The position of the section is outlined in Fig. 1.

# Kristin Field. Porosity preservation due to chlorite and illite coatings

Storvoll et al. 2002

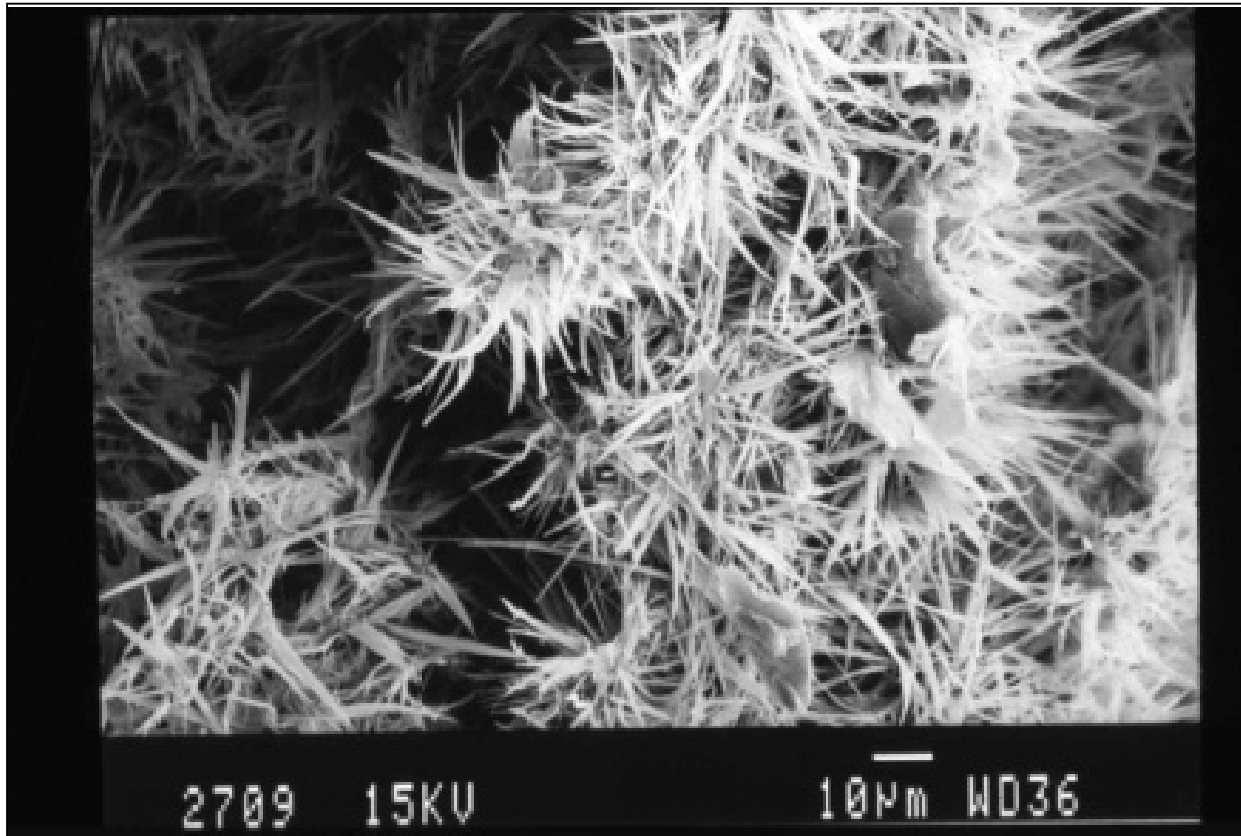


Garn Fm.  
4.8 km

Fig. 9. (a) Illite with a corn flake morphology, which implies a smectite mixed layer clay precursor (Pollastro, 1985). Well 6406/2-3T3, 4670.8 m (core depth). (b) Illite with a more sheet like morphology compared to (a). Well 6406/2-3T3, 4701.5 m (core depth).

Fig. 10. (a) Coating of illite and chlorite (Ill./chl. coat.). Backscatter electron image. Well 6406/2-5, 4846.8 m (core depth). (b) Backscatter electron image of continuous chlorite coating (Chl. coat.). Well 6406/2-5, 4846.8 m (core depth).

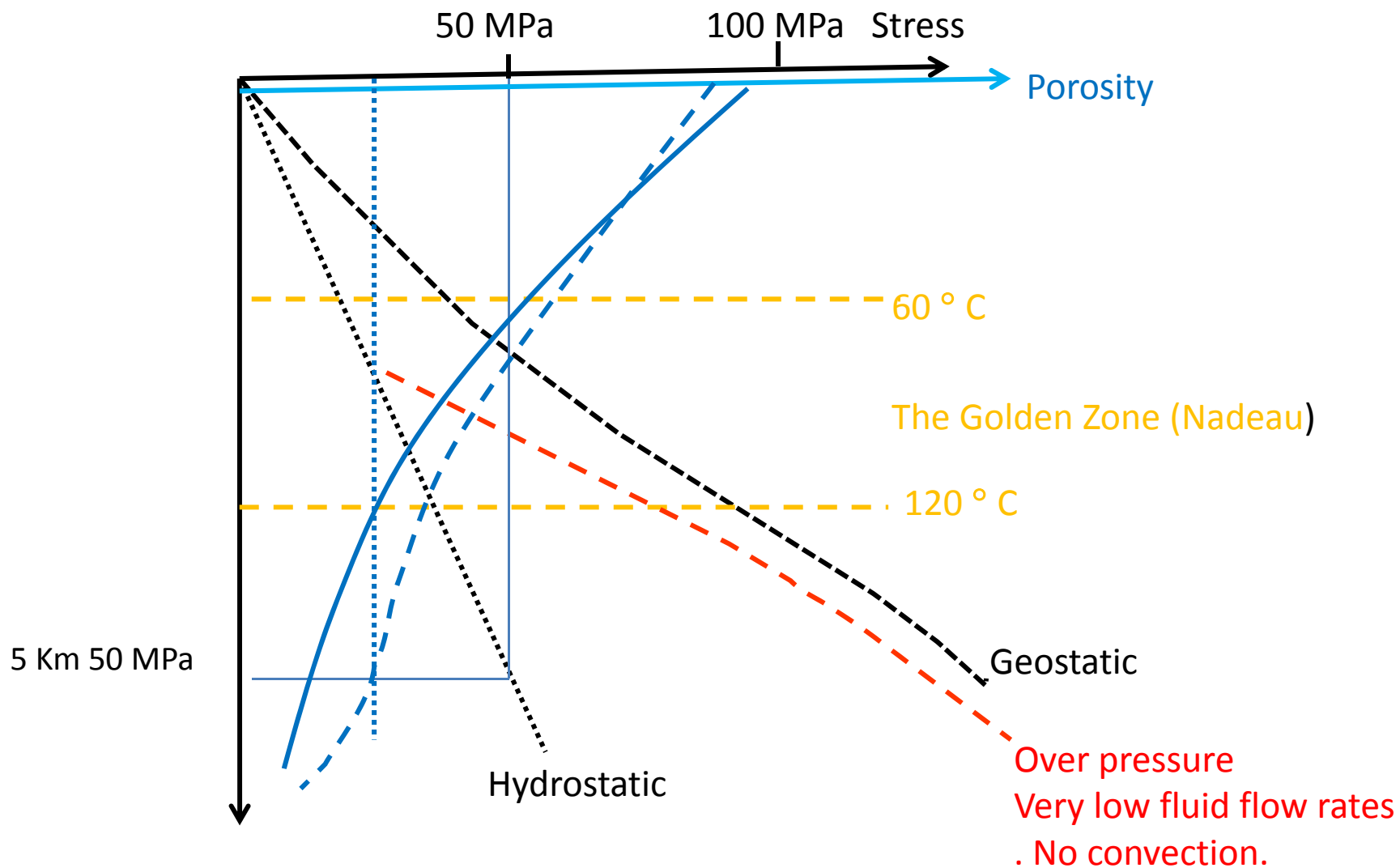
# Pore filling illite



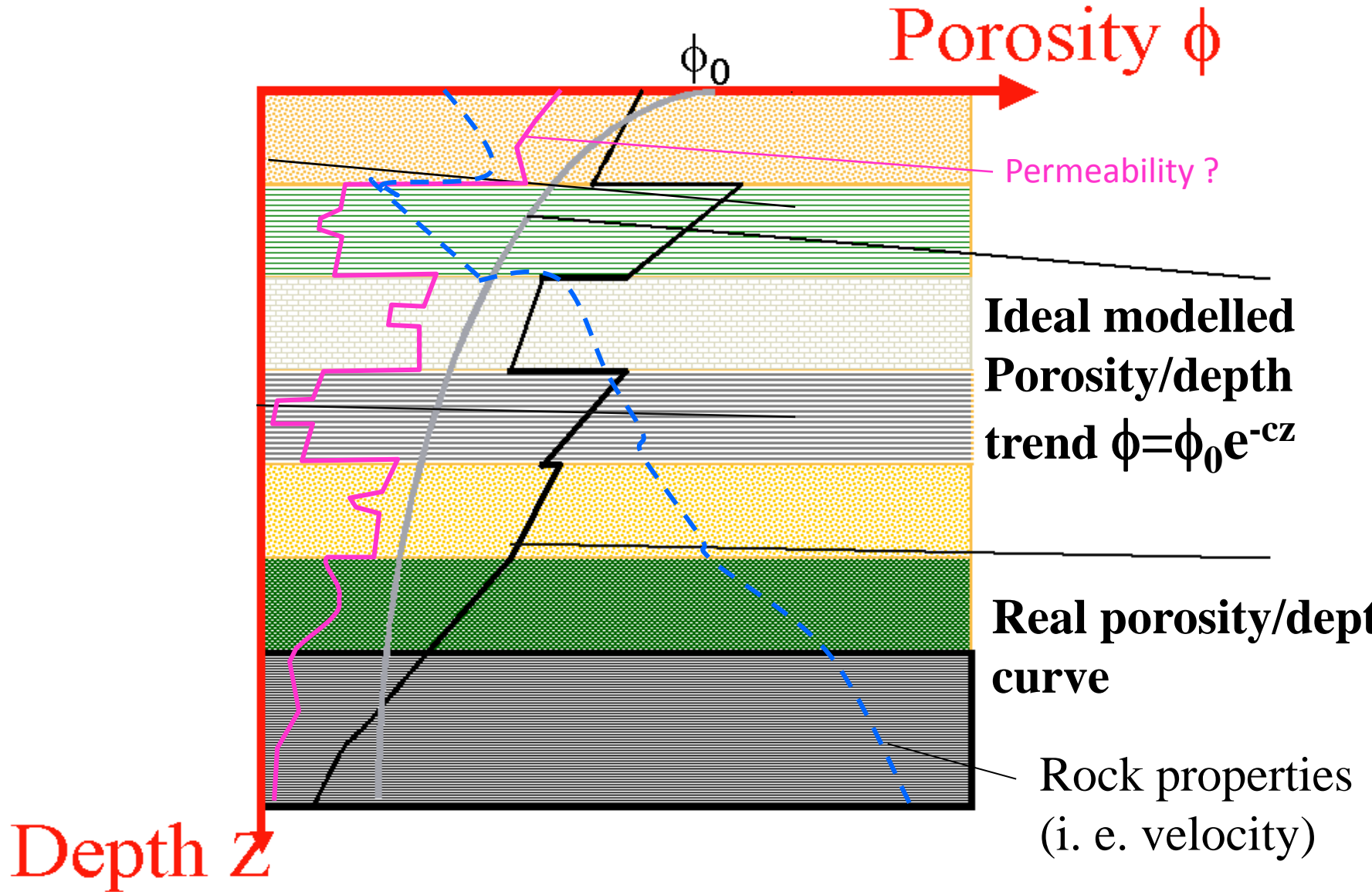
Pore-filling authigenic illite from a Jurassic reservoir, Haltenbanken (4.2 km depth)

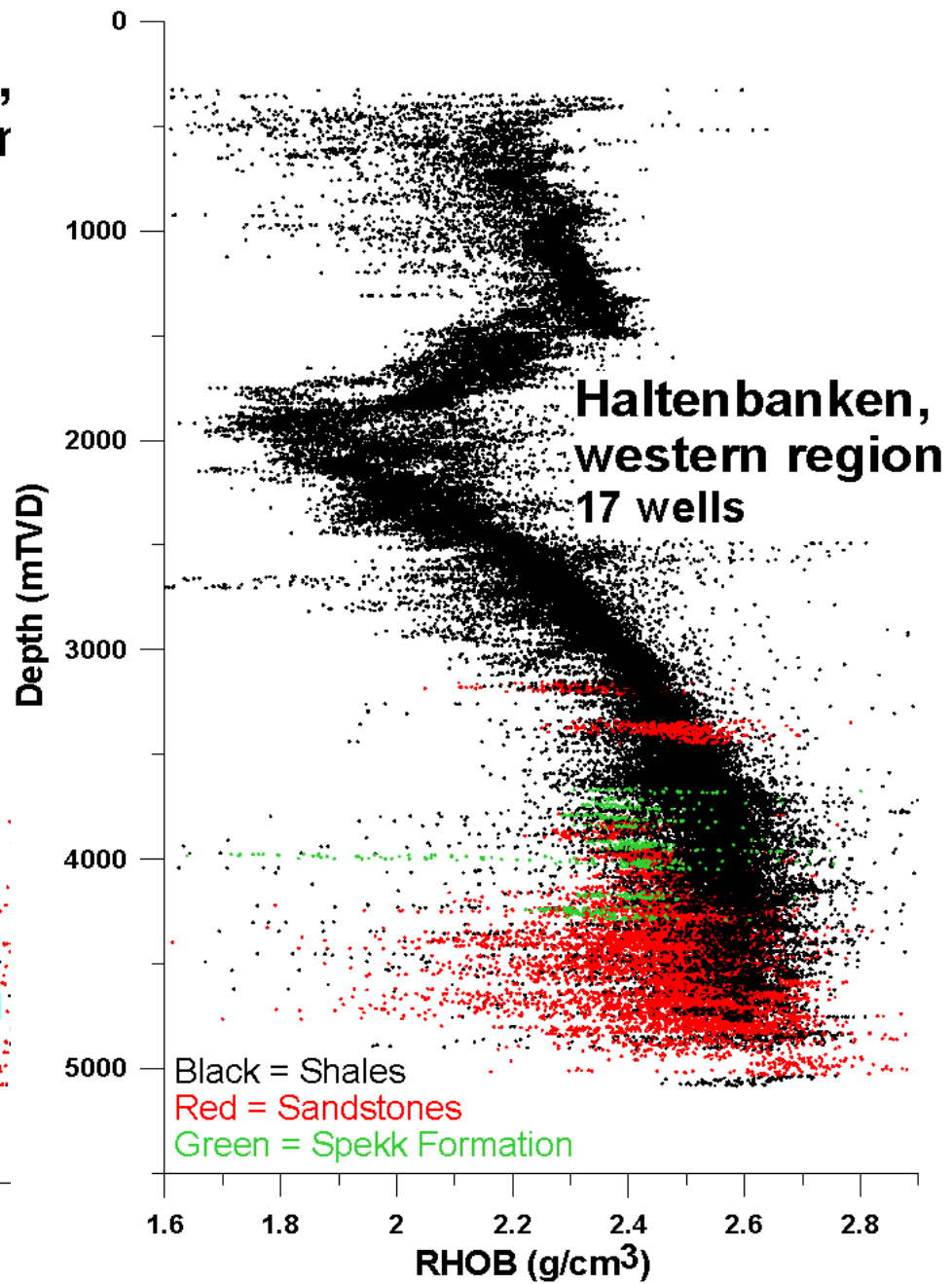
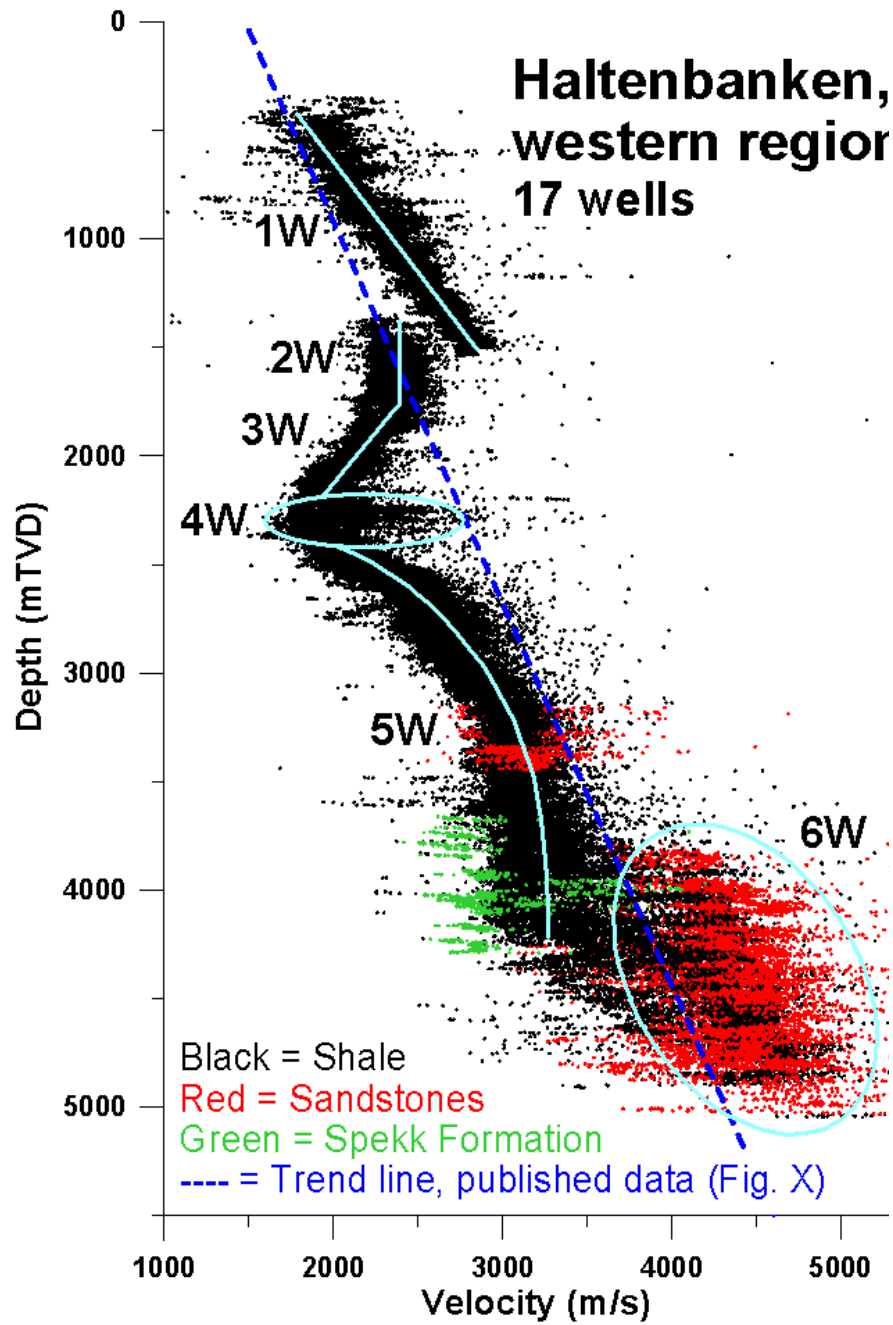
• kaolinite + K-feldspar = Illite + quartz + water  
( $>130\text{ }^{\circ}\text{C}$ )

K. Bjørlykke, Department of Geosciences



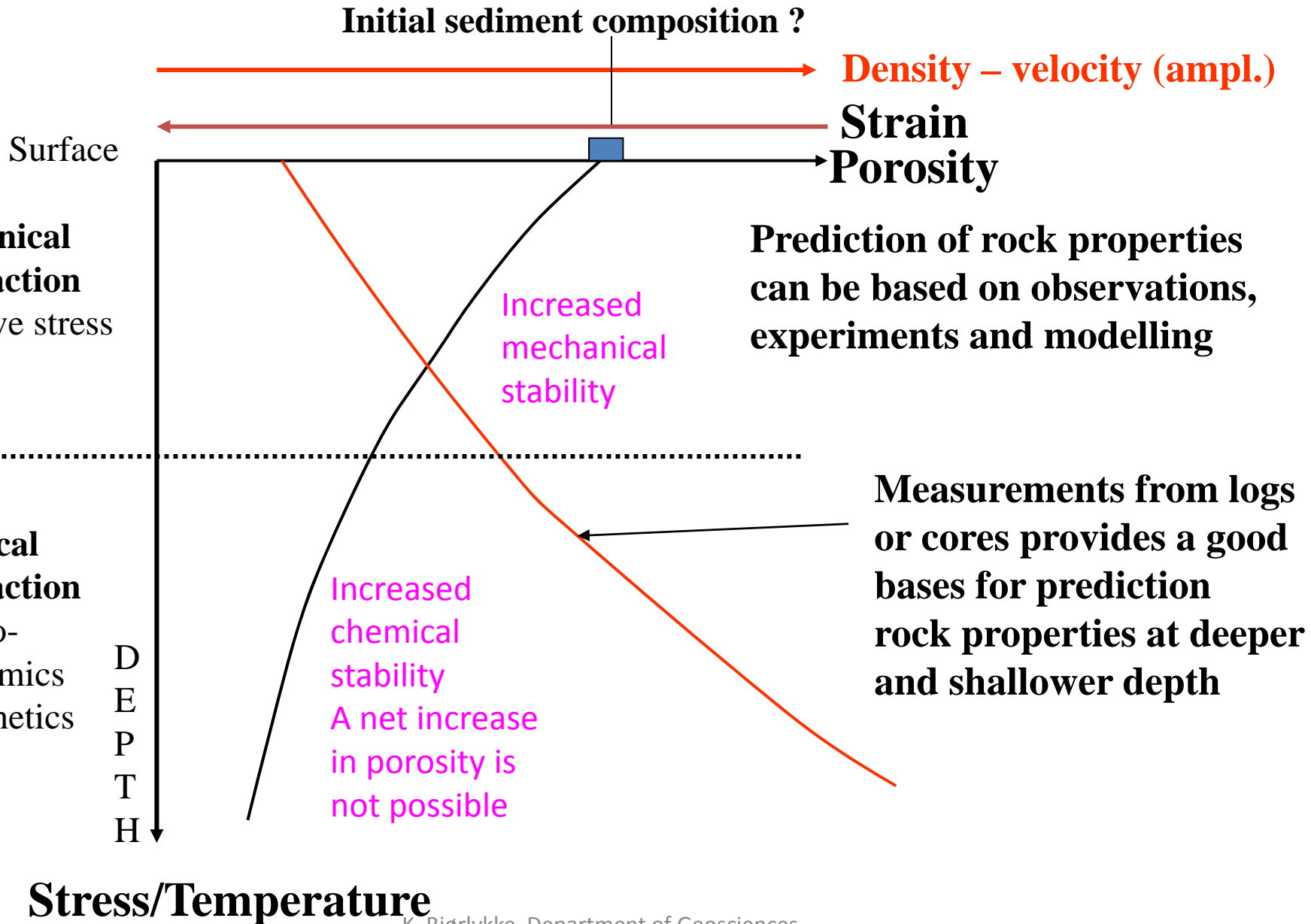
# Compaction of sedimentary layers with different initial composition.



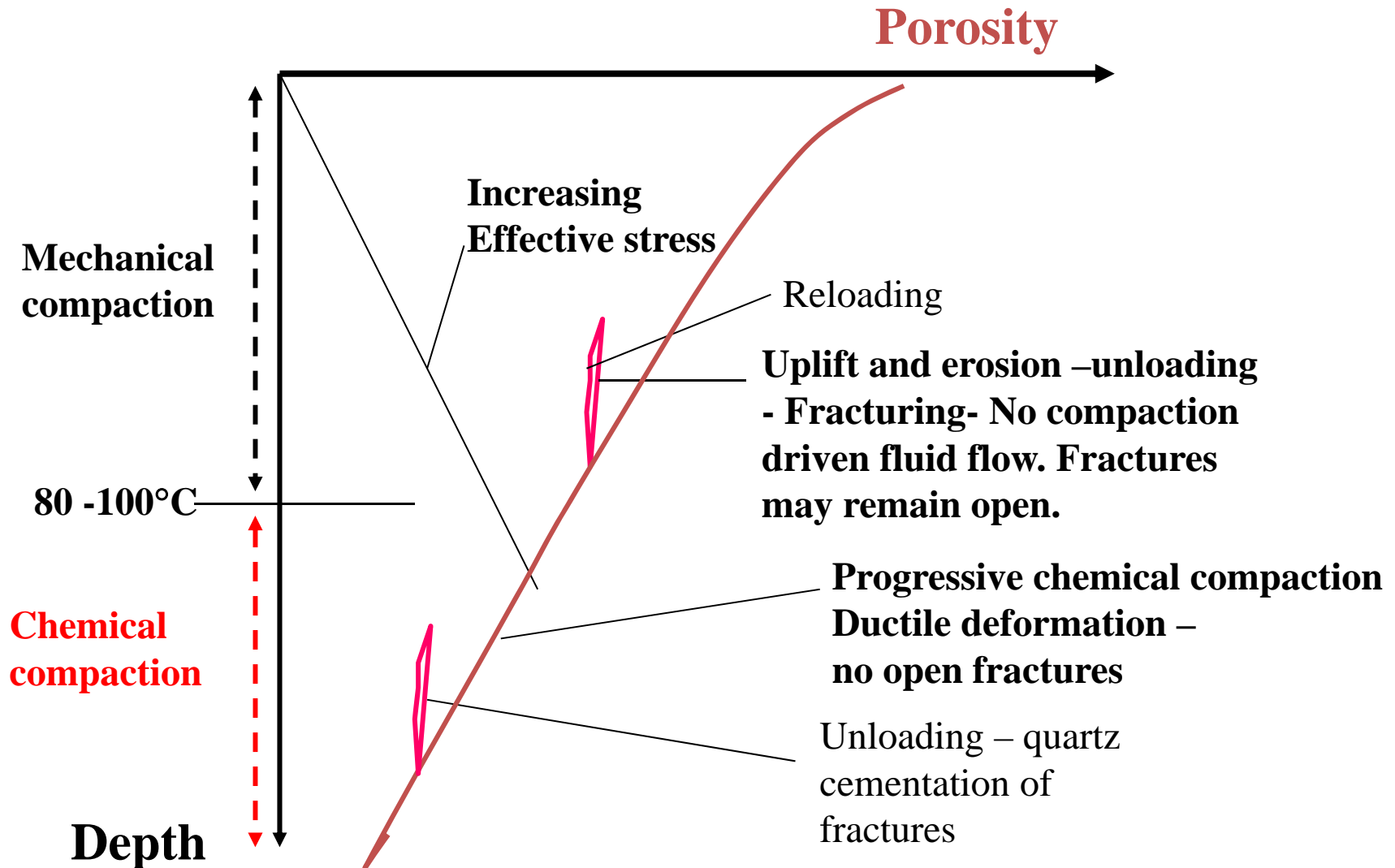




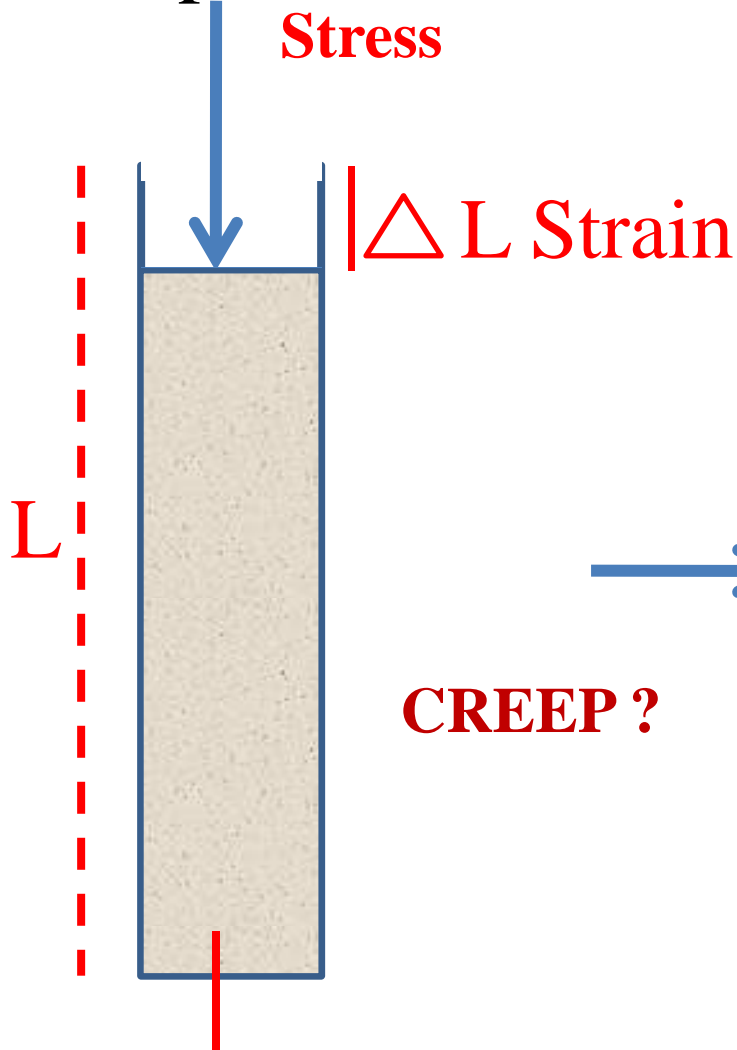
# Burial diagenesis - Compaction of silicious sediments



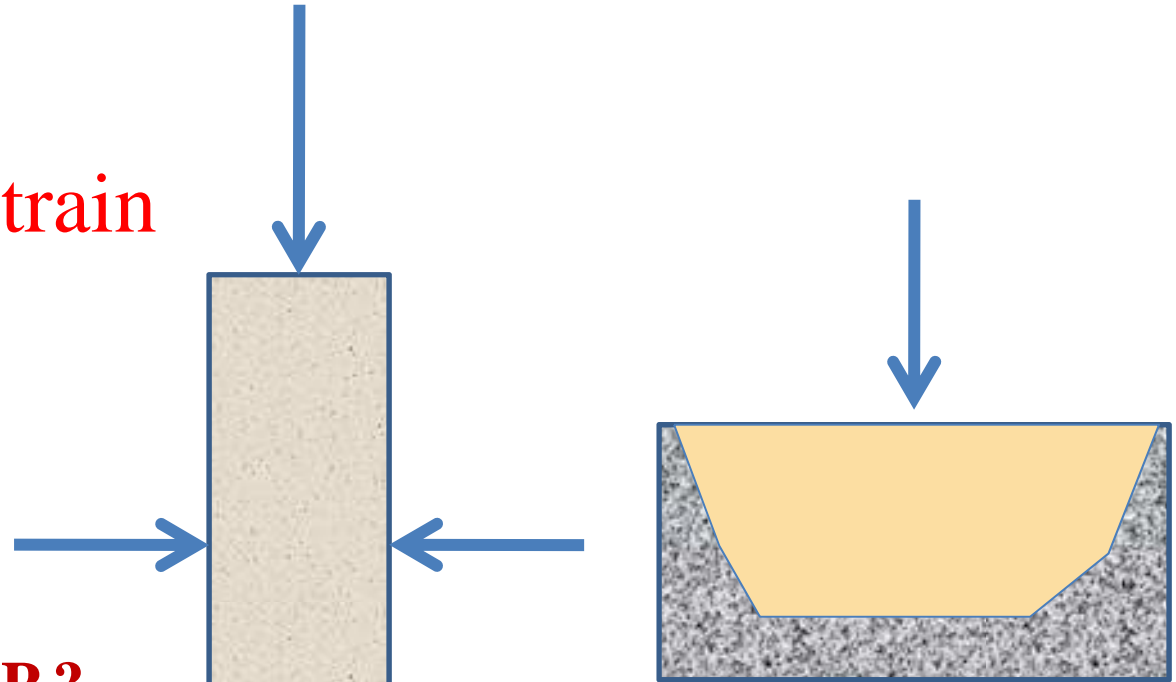
# Mechanical and chemical compaction during progressive burial and uplift



# Experimental mechanical compaction



# Compaction in Sedimentary basins



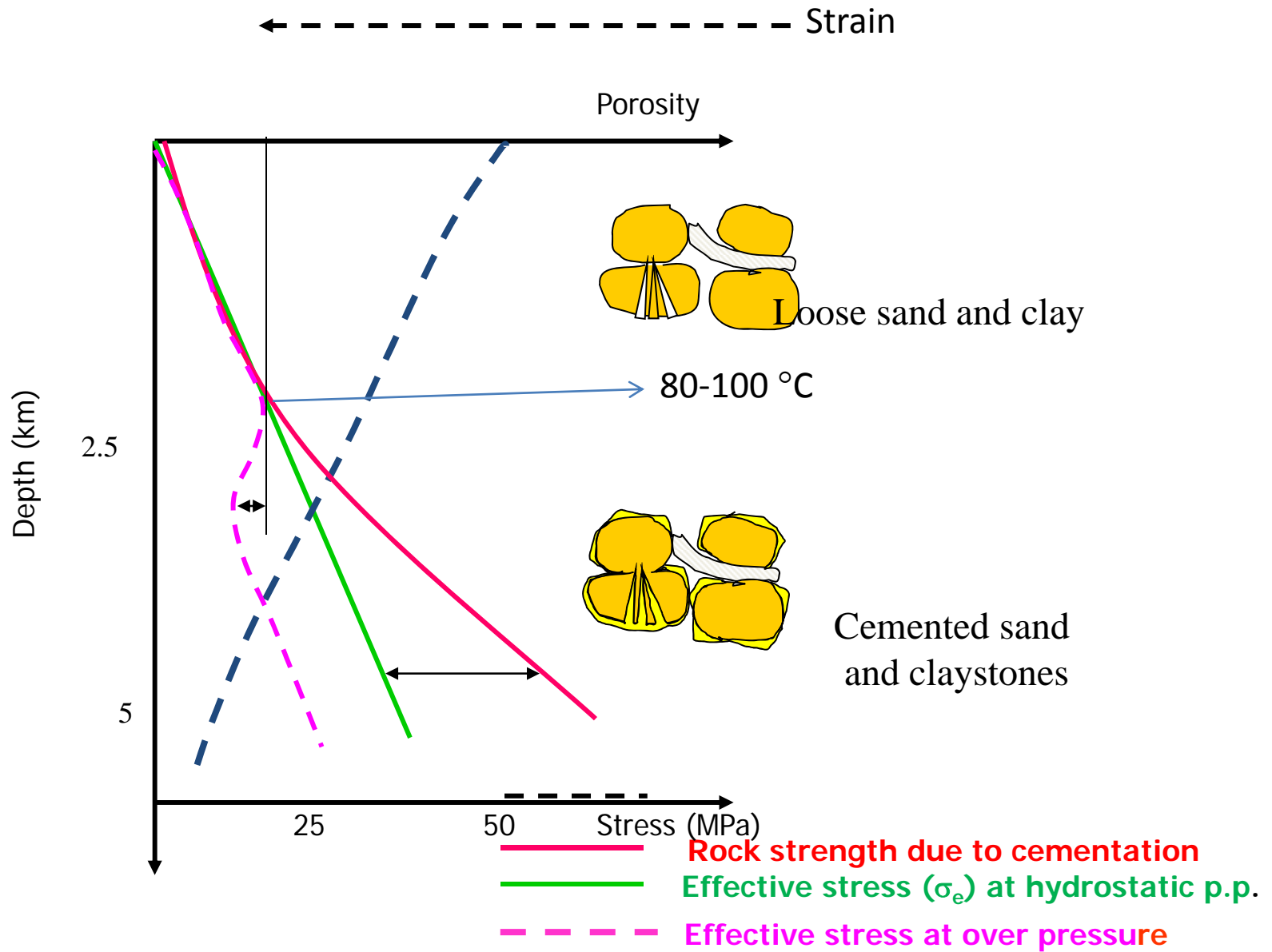
**CREEP ?**

Sedimentary basin-  
mainly vertical  
compression

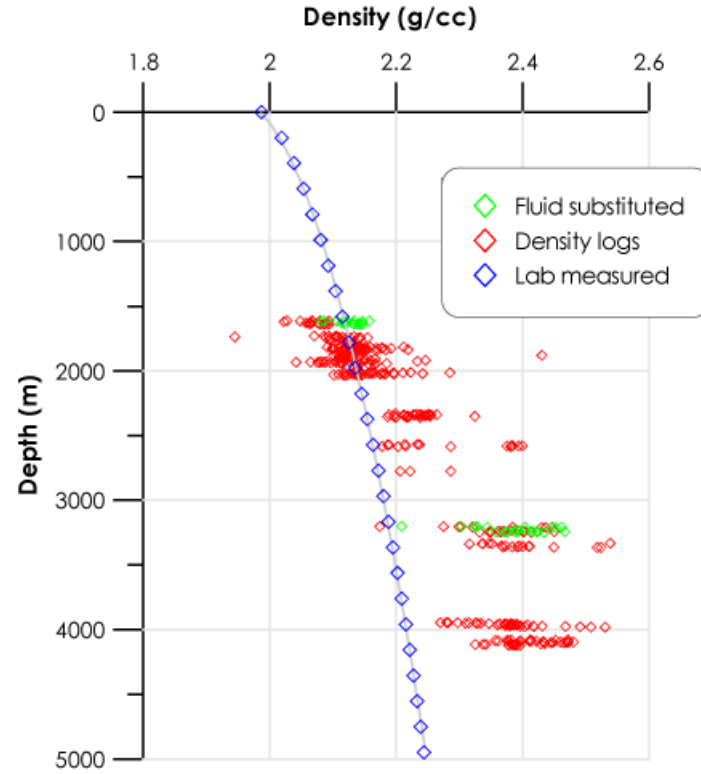
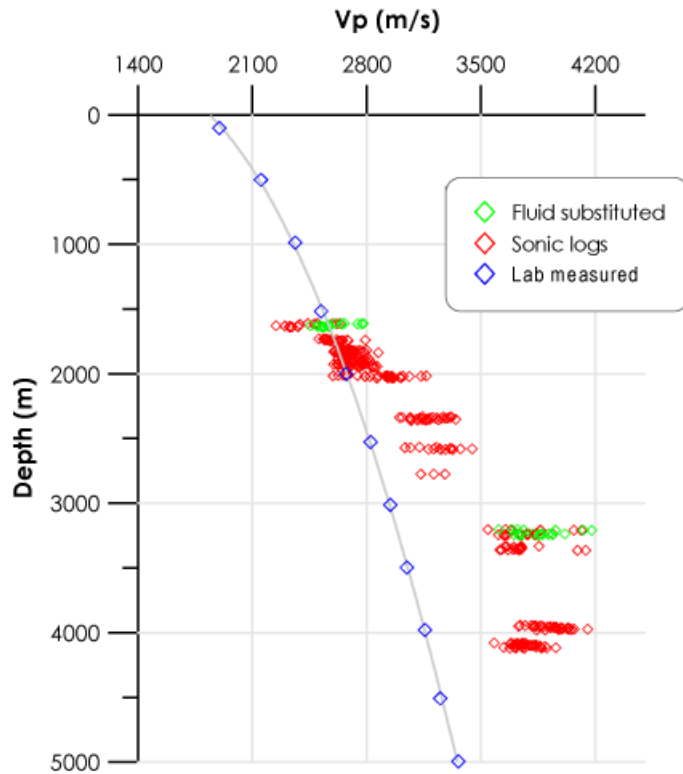
Oedometer

Triaxial compaction

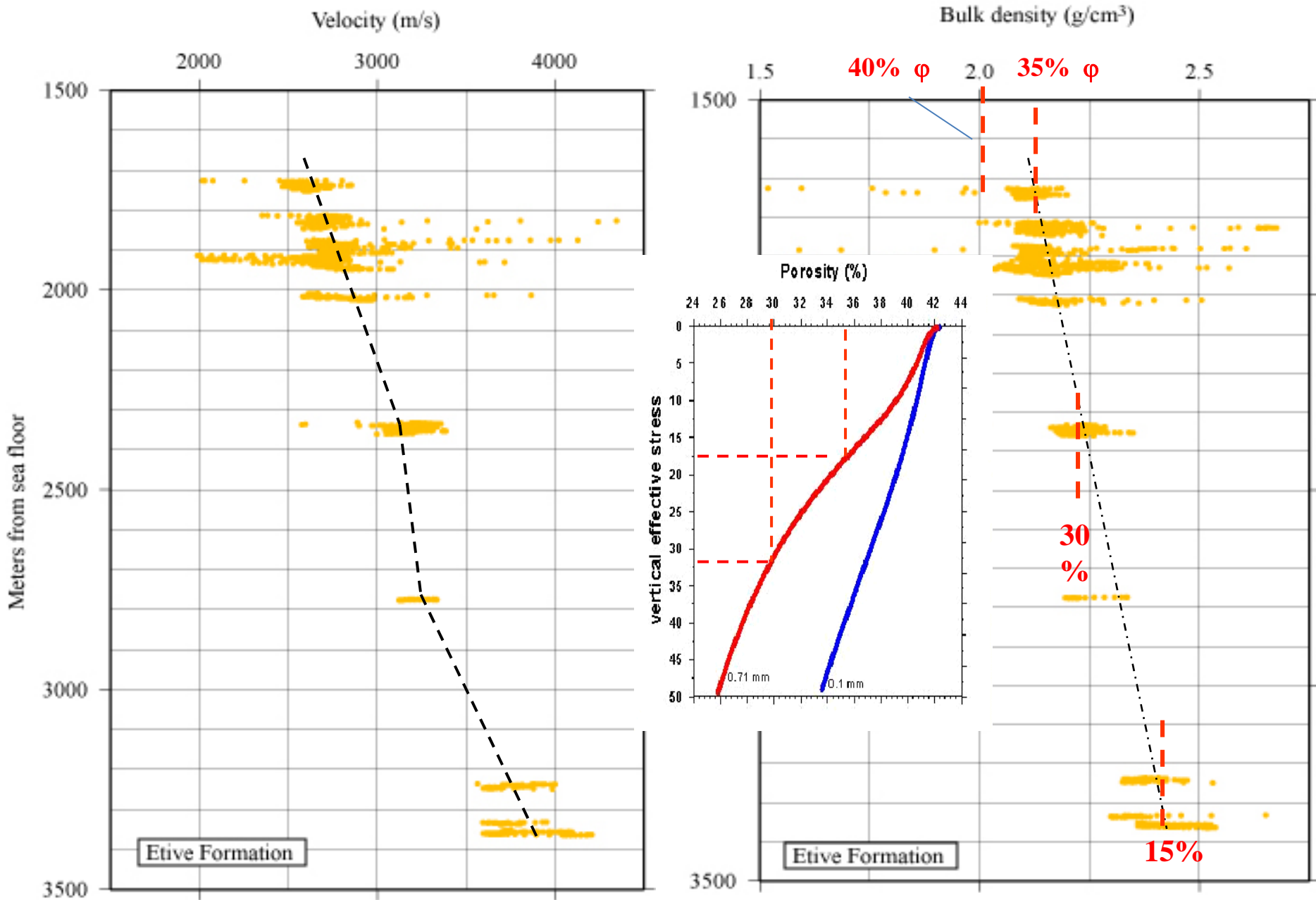
# Compaction of Sand

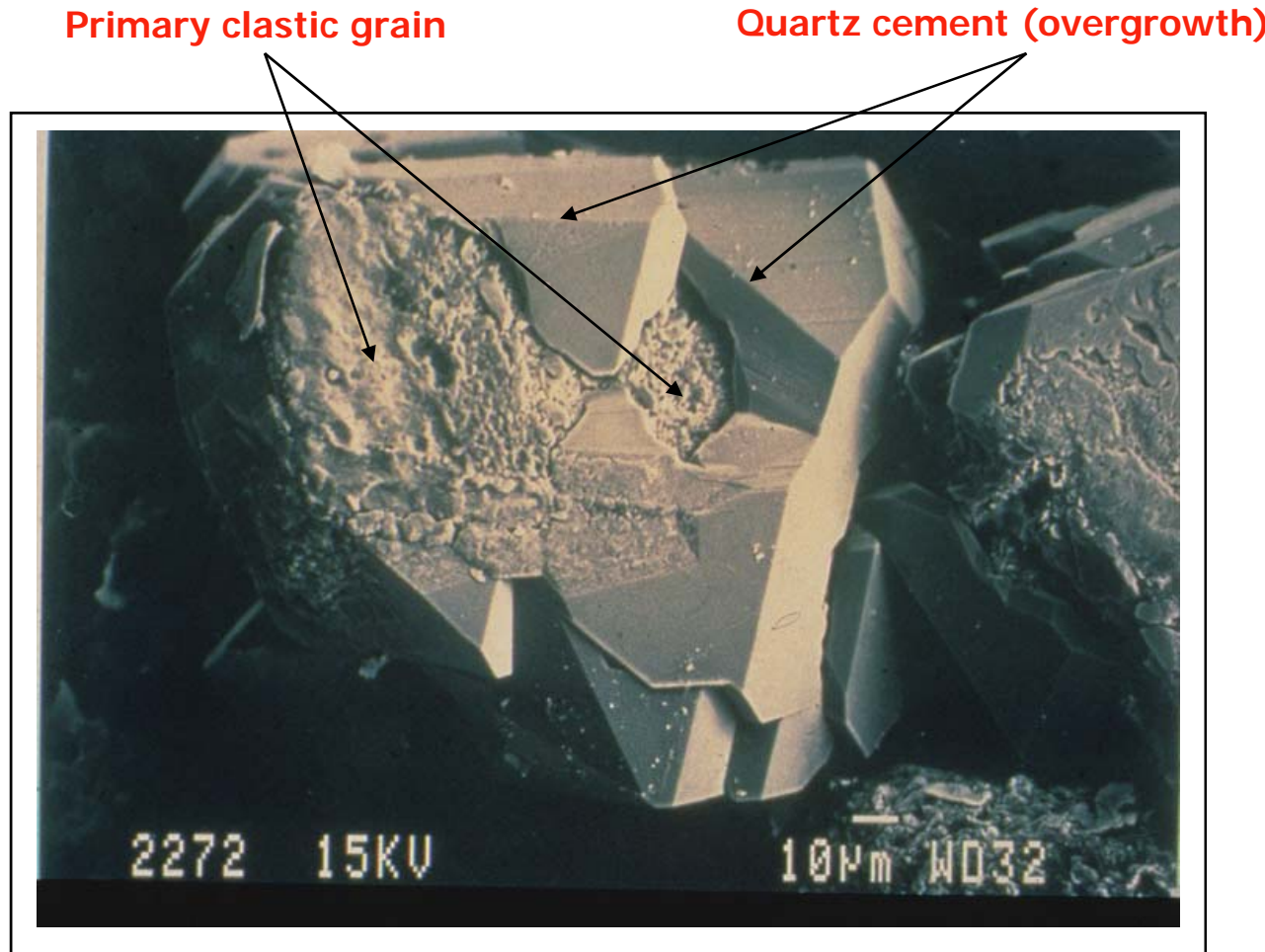


# Sandstones – Etive Formation



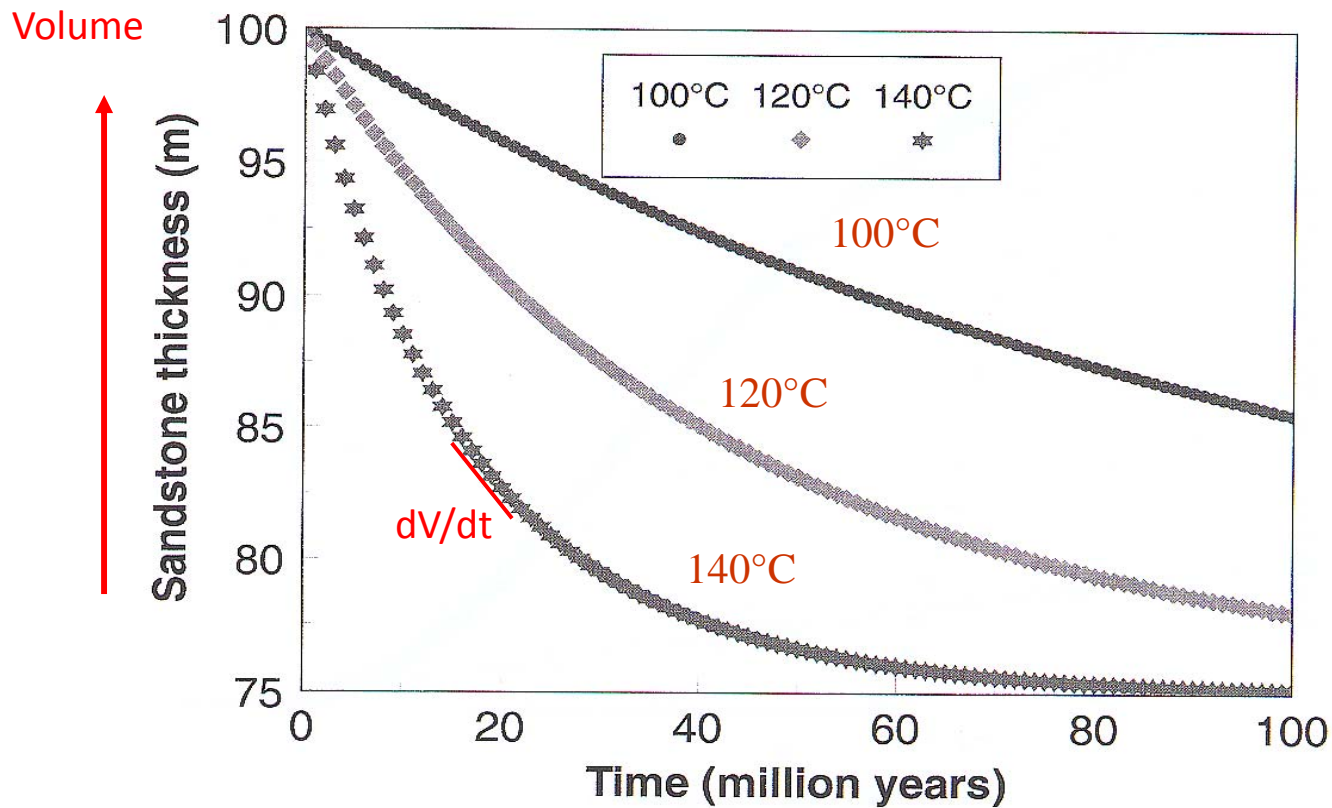
# Etive Fm velocity and density as a function of depth





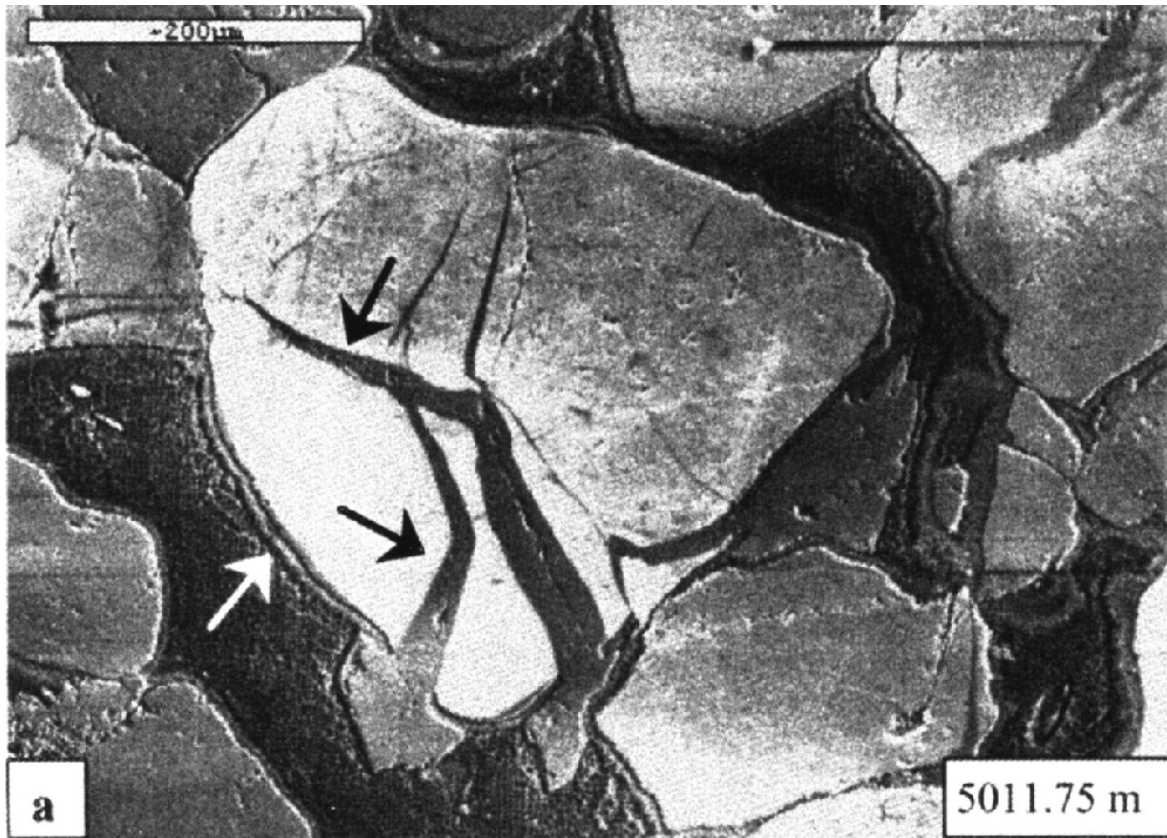
Quartz cement with smooth crystal surfaces as overgrowth on clastic grains

# Compaction due to quartz cementation at constant temperature



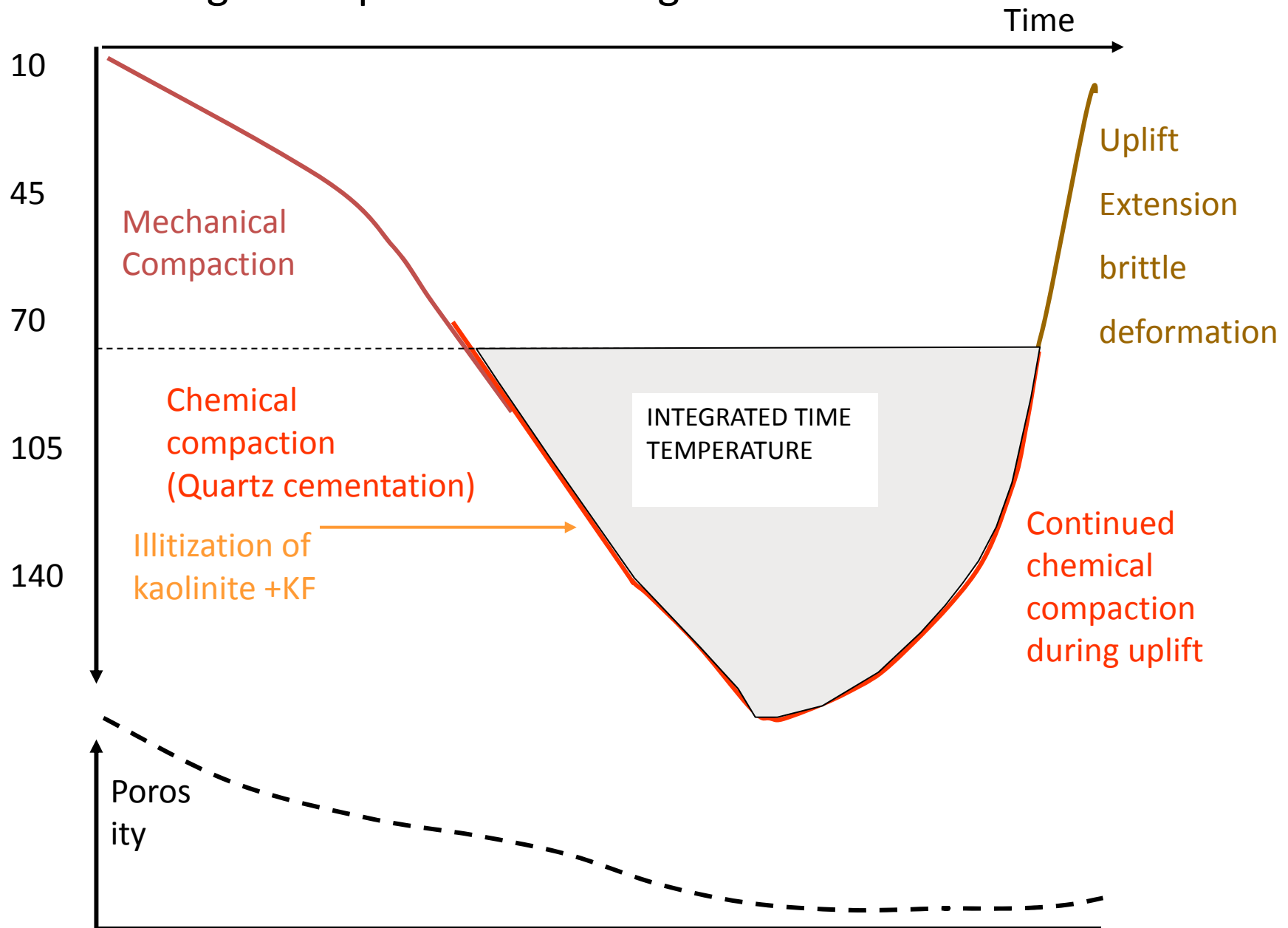
Walderhaug et. al 2001



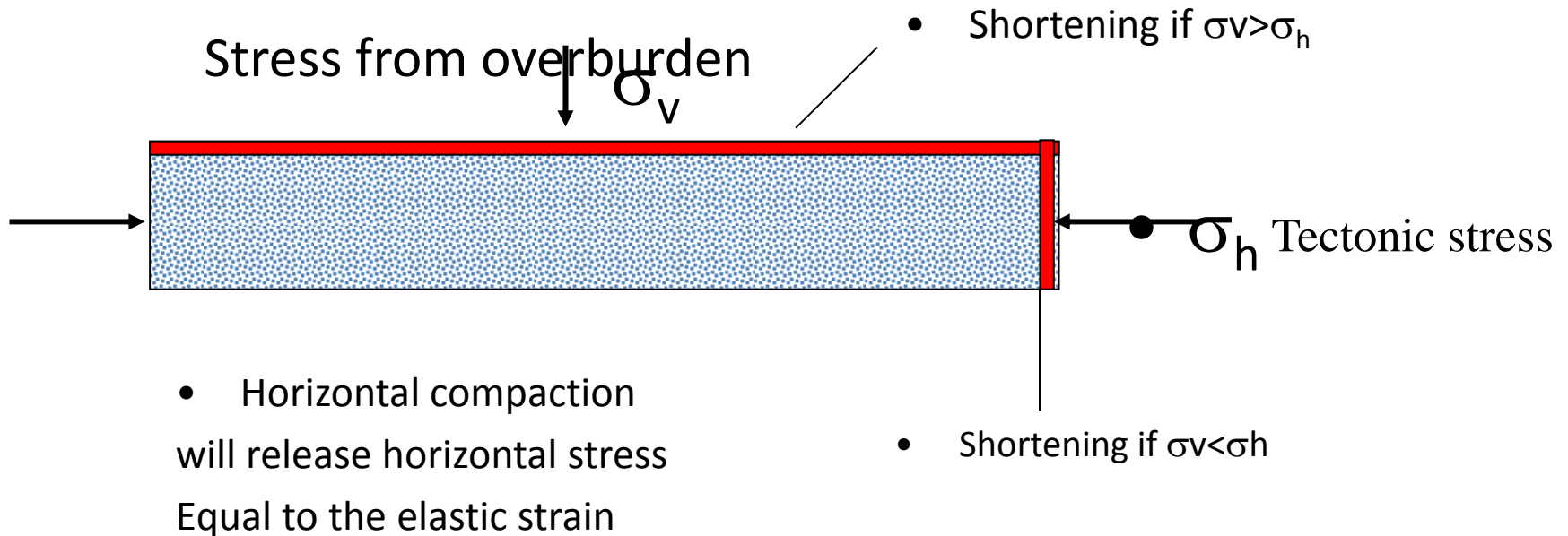


Natural fractures in reservoir sandstone (Tilje Fm, Smørbukk Field). The quartz grains are chlorite coated but quartz cement have grown from fractured quartz From Chuhan et al. 2002

# Diagenetic processes during burial.



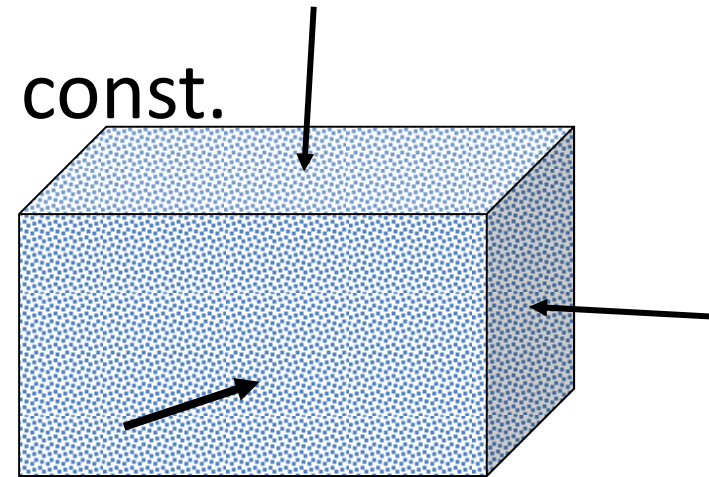
# Vertical or horizontal compaction

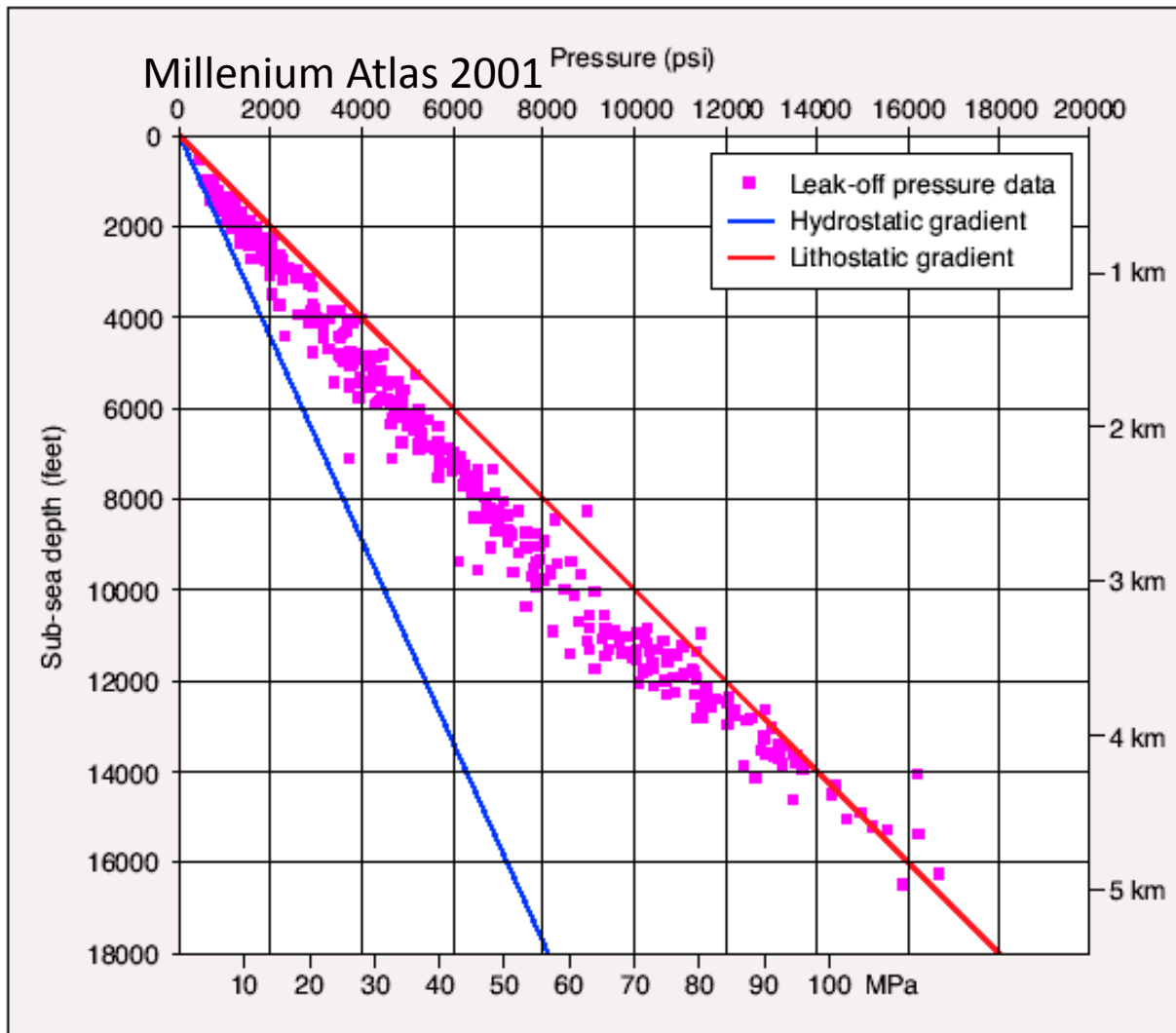


- If the basement is shortened the overlying sediments will compact horizontally and the horizontal strain will reduce the build up of horizontal stress

# Sediment compaction – rock shrinkage

- Bulk modulus = Stress/strain( $\Delta V$ )
- If the strain  $\Delta V$  is 0.001 or 0.1 % and the Bulk modulus is 50G Pa the effective stress is reduced by 50 MPa
- k volume ( $V_R$ )= Solids ( $V_S$ )+ Fluids (porosity)
- Void Ratio =  $V_S/V_f = \phi / (1 - \phi)$
- For isochemical reactions  $V_S = \text{const.}$
- $\Delta V = \Delta \phi$  ,  $dV/dt = d\phi/dt$





Leak off pressures suggest that the horizontal stress is close to the vertical overburden stress

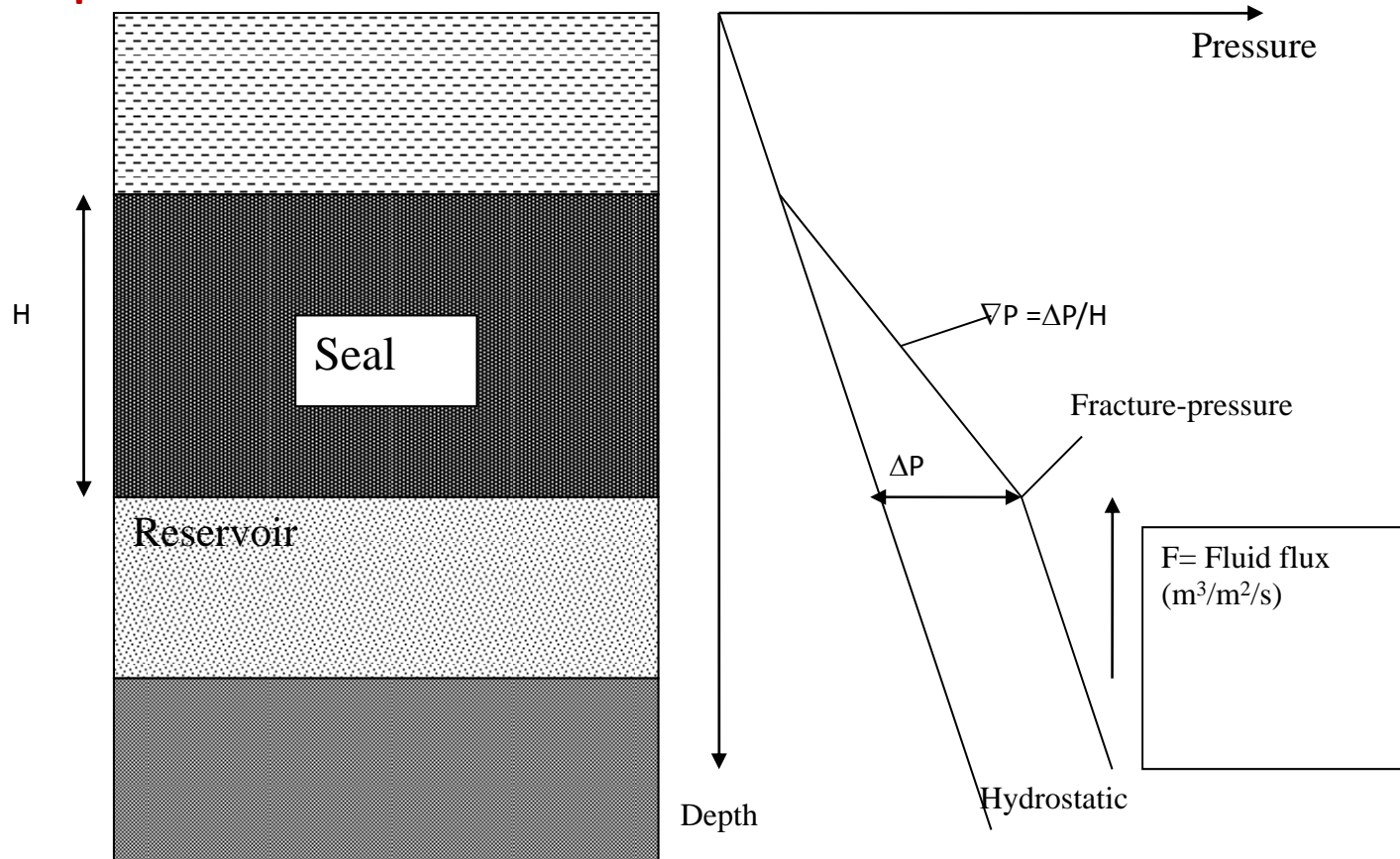
Figure 18.6

**Central North Sea fracture gradient.**

The fracture-pressure gradient is the pressure required to generate fractures where the minimum stress (usually the horizontal stress) and the tensile strength of the rock are exceeded by the pore pressure. In the North Sea, the fracture gradient is slightly less than the lithostatic gradient. The fracture gradient can be identified

by plotting leak-off test data against depth. In this figure the data for several wells from the central North Sea are plotted. Given the principle of the leak-off test, the data show that in the North Sea the minimum stress is horizontal and constitutes about 85% of the vertical stress, increasing to 95% or more at depths below about 4 km. See Grauls (1997).

**At great depth the compaction driven fluid flux is very low but the permeabilities of shales are close to zero**

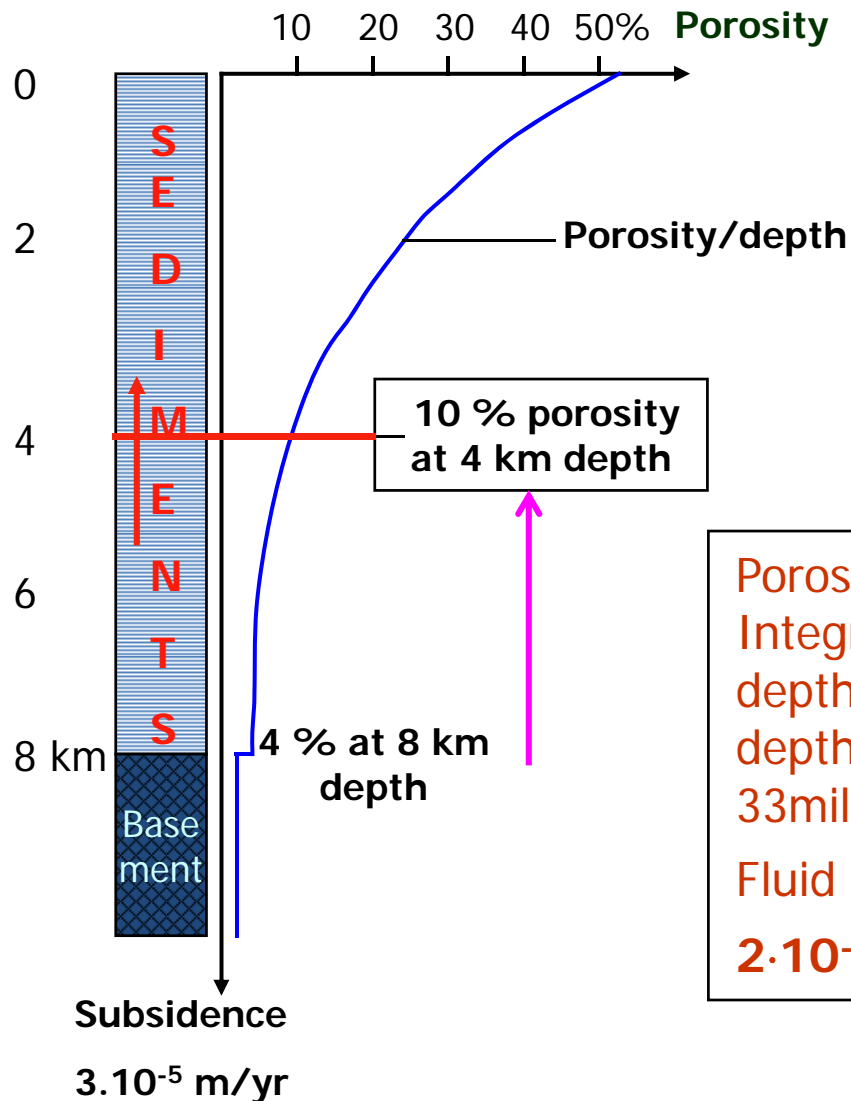


$$F = \left( \int_{z_1}^{z_2} \frac{\partial \phi}{\partial z} dz \right) \cdot \frac{\partial z}{\partial t}$$

Sedimentation rate  $2 \cdot 10^{-5}$  m/yr  
 Flux =  $1.5 \cdot 10^{-13}$  m<sup>3</sup>/m<sup>2</sup>s  
 Permeability(k) = 0.01 nD

**$F = k \cdot \nabla P / \mu$  At greater depth the compaction driven flux is a function of temperature rather than effective stress At constant viscosity k and  $\cdot \nabla P$  vary inversely.**

# Compaction driven fluid fluxes in the deeper parts of sedimentary basins

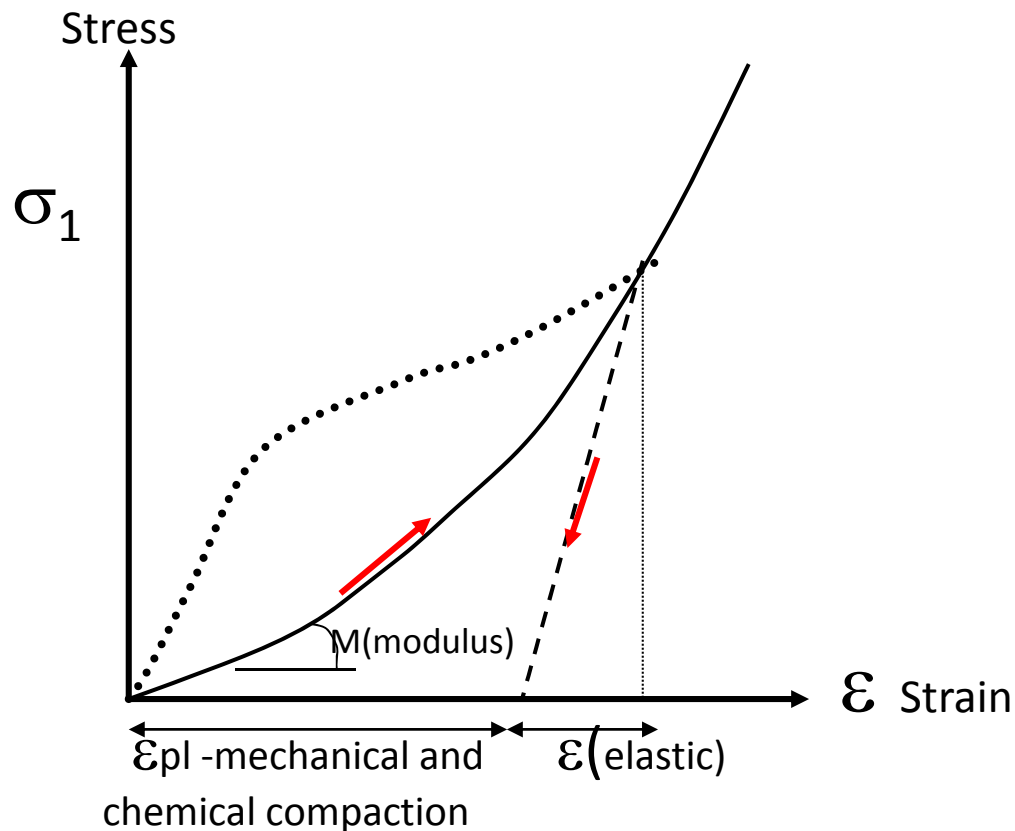


$F = k \cdot \nabla P / \mu$   
*The compaction driven flux is relatively constant over time*

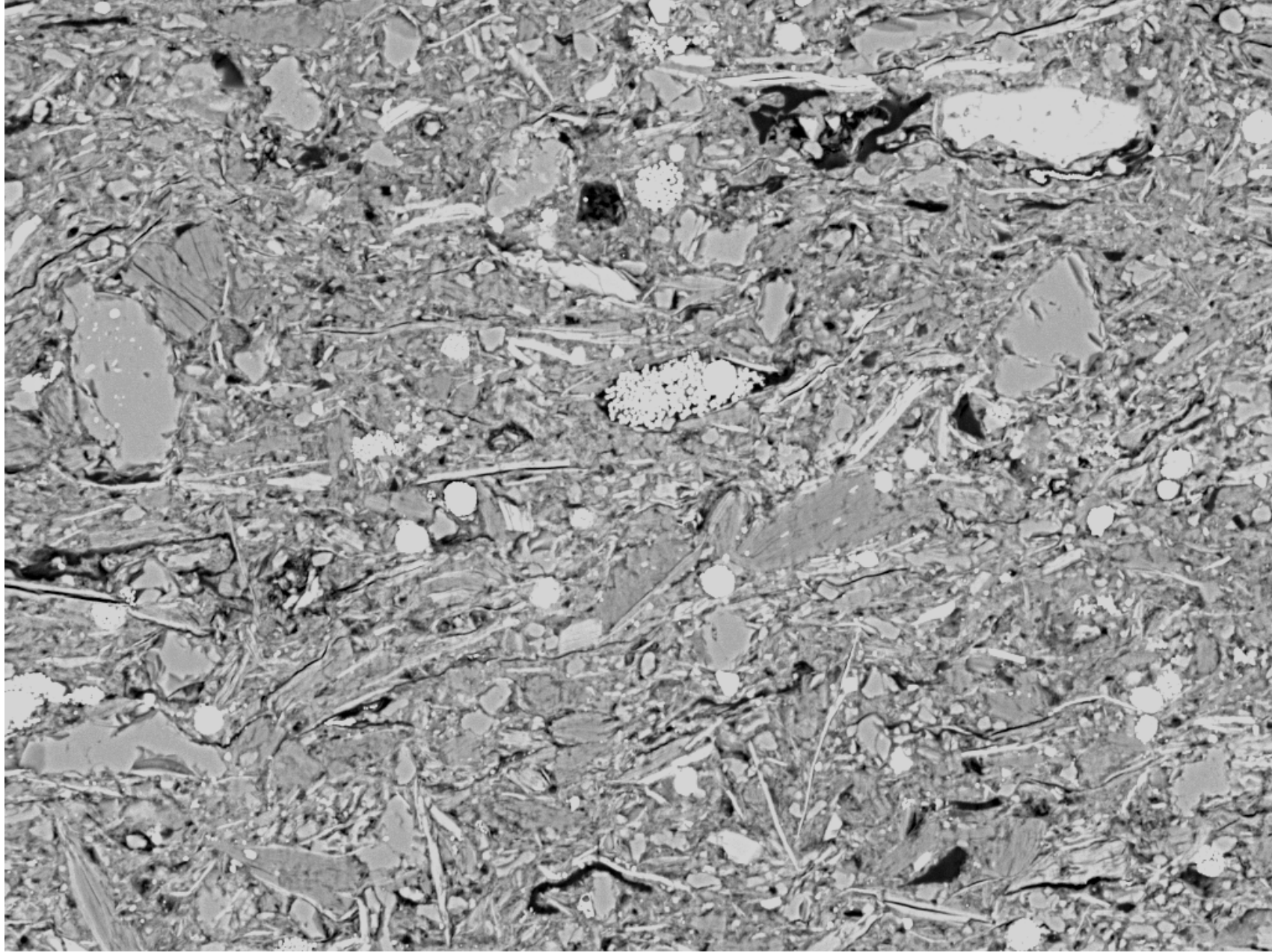
Porosity loss/km subsidence 1.5%  
 Integrated flux (from 4-8km depth) pr km subsidence at 4 km depth: Total flow  $60 \text{ m}^3/\text{m}^2$  over 33mill years.  
 Fluid flux =  $60 \text{ m}^3/\text{m}^2 / 33 \cdot 10^6 \text{ yr} = 2 \cdot 10^{-5} \text{ m}^3/\text{m}^2 \text{ yr}$ .

# Compaction

- Elastic Stress/strain compared with mechanical ductile strain and chemical strain.



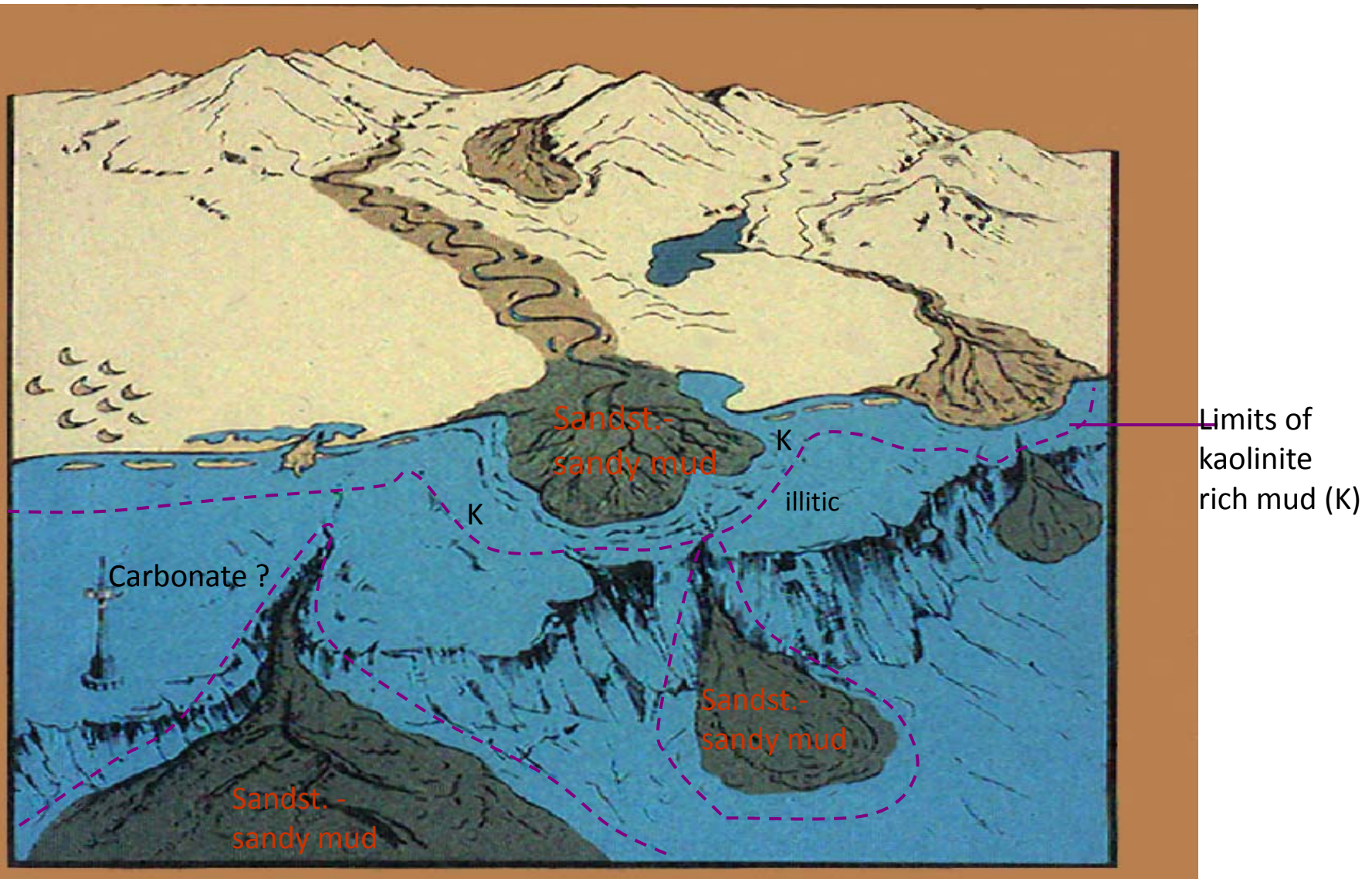




100 $\mu$ m

6506/11-7 4479,33m Lange

$E_{50}=13,77\text{GPa}$   $\mu_{50}=0,53$   $V_p=4118\text{m/s}$   $V_s=2001\text{m/s}$



The properties of sedimentary rocks are a function of provenance, depositional environment and diagenesis.

# Conclusions

**The physical properties of sedimentary rocks change continuously during progressive burial and also during uplift and unloading.**

**Prediction of the distribution of rock properties must be based on the primary sediment composition and the burial histories.**

**Experimental compaction of sand and clay helps to predict the physical properties of sandstones and mudstones at moderate depths.**

**Experimental compaction of carbonates may simulate both mechanical and chemical compaction.**

**Compaction processes are also important for the permeability reduction in shales (cap rocks) and quartz cementation here plays an important role.**

**The inversion from geophysical data, (including EM data) to rock properties and fluid saturation requires a better data base for rock properties as a function of mineralogy and textural relationships.**