





NPD FORCE Geophysical Methods Group

Survey design & modelling



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General BHS Survey Design & Modelling Guidelines

1. Survey Objectives:

- Time-depth velocity control \rightarrow is boat required for deviated wells?
- Wideband, true-amplitude, zero-phase → optimize source parameters?
- Look-ahead / drilling assistance \rightarrow depth accuracy or thickness resolution required ?
- High-resolution imaging (P- or converted S-waves) → resolution, lateral illumination and fold?
- AVO/AVAZ calibration \rightarrow offset/angle ranges required, antenna position
- TTI anisotropy \rightarrow global travel times or local slowness-polarization?
- Full Waveform inversion \rightarrow which parameters we want to invert?
- Fractures characterization \rightarrow HTI, ORT or lower symmetry media
- Seismic multiples study \rightarrow 1D reflectivity modelling
- Time-Lapse response → rock physics / geomechanics
- Microseismic monitoring → minimum magnitude detectable, MT invertibility, ...

2. Geological model/velocity model complexity

- Flat and boring or high dips? Nearby faults, gas pockets or salt domes ?
- Are there strong lateral or vertical velocity variations?
- Is there a preferential dip direction to shoot 2D survey?



General BHS Modelling Guidelines (cont.)

- 3. Input data available: *quantity and quality*
- 4. Modelling technique: conditioned by all three previous points
- 5. Well conditions & well geometry: type of tool or fiber optics and conveyance
- 6. Surface conditions: where sources can be deployed
- 7. Equipment available: if not in place, feasibility to import equipment in time
- 8. **Project cost:** any technical solutions must be realistic & cost-effective



Pre-survey Geophysical Modelling: Feasibility & Geometry Optimization

- Illumination, fold, incidence angles at targets <u>& at fiber</u>
- Anisotropic synthetics and moment tensor sources
- Low-frequency strain modeling vs DAS data







Omega 3D visco-elastic anisotropic Finite Differences used in complex surveys

DAS box frequency response can be applied to synthetics



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Standard Zero-offset VSP design

- 3C / 4C sensors spaced @15 m (5 30 m) For DAS fiber optics, @5m (1 - 10 m)
- Irregular spacing is OK
- To avoid aliasing spacing: DZ < Vmin / 2* Fmax
 E.g.: P-waves, Vmin = 2250 m/s and Fmax = 75 Hz → DZ < 15 m
 Higher frequencies, fine layering, complex geology, S-wave or tube waves require shorter spacing (~7.5 m)
- Aliasing avoided with median filters when the downgoing & upgoing moveouts are known
- Short spacing is recommended for high resolution applications, higher SNR results and also in complex geology with rich content of different wavefields
- VSPs can be recorded in OH or CH, fair cementation required over near vertical sections. No cement required if deviation > ~30°
- Standard VSP program: record at 15 m from TD up to as shallow as possible (no ringing on Z-axes) and then at ~120 m up to surface (or seabed) if data quality allows









Fundamentals of Borehole Seismic Technology (Kelsall, Rufino & Guerra, 2022)

• 3C

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Rig source or boat VIVSP?

- Well step-out > ~500 m?
- Flat and boring geology?
- Propagation angles high?
- Velocity variations strong?
- Anisotropy high?

Vertical OWT Difference VSP - VIVSP





Test accuracy of isotropic straight ray path assumption

Standard Method: Cosine Correction



The correction assumes straight seismic ray paths

 \rightarrow The field computations ALWAYS use this method

Examples of T-Z listing in field reports:

Stack Summary Listing (1/6) Survey WAVEFIELD_RECEIVER_Z_for_Report.ldf

| | Stack Number | Measured Depth [ft] | True Vertical Depth [ft] | Measured Time [s] | One-way Vertical Time [s] | Two-way Vertical Time [s] | Interval Velocity [ft/s] | Average Velocity [ft/s] | RMS Velocity [ft/s] |
|---|-----------------|------------------------|-----------------------------|----------------------|---------------------------------|---------------------------------|-----------------------------|----------------------------|---------------------------|
| Ī | | 0 | 0 | 0 | 0 | 0 | | | |
| ĺ | | | | | | | 5388.3 | | |
| | 43 | 391.0 | 345.0 | 0.0772 | 0.0640 | 0.1280 | | 5388.3 | 5388.3 |
| | | | | | | | 6479.9 | | |
| | 43 | 441.0 | 395.0 | 0.0830 | 0.0717 | 0.1435 | | 5505.7 | 5516.1 |
| ĺ | | | | | | | 7242.3 | | |
| | 43 | 491.0 | 445.0 | 0.0883 | 0.0786 | 0.1573 | | 5658.2 | 5688.7 |
| | | | | | | | 7403.8 | | |
| ĺ | 43 | 541.0 | 495.0 | 0.0938 | 0.0854 | 0.1708 | | 5796.2 | 5842.7 |
| | | | | | | | 6608.5 | | |
| | 42 | 791.0 | 745.0 | 0.1282 | 0.1232 | 0.2465 | | 6045.6 | 6088.1 |
| | | | | | | | 7747.9 | | |
| | 42 | 841.0 | 795.0 | 0.1341 | 0.1297 | 0.2594 | | 6130.3 | 6181.2 |
| | | | | | | | 9031.1 | | |
| | 42 | 891.0 | 845.0 | 0.1392 | 0.1352 | 0.2704 | | 6249.1 | 6323.2 |
| 1 | | 1 | 1 | | 1 | 1 | | 1 | |

Stack Summary Listing

| Stack number | Well depth[m] | TVD from SRD[m] | TT[ms] | TT(TVD Corrected)[ms] | TWT(TVD Corrected)[ms] | Interval Velocity[m/s] | Average Velocity[m/s] | RMS Velocity[m/s] |
|-----------------|---------------|--------------------|--------|--------------------------|---------------------------|---------------------------|--------------------------|----------------------|
| 62 | 49.99 | 39.06 | 91.07 | 31.29 | 62.59 | 983.77 | 1248.08 | 1248.08 |
| 61 | 51.54 | 40.61 | 92.47 | 32.87 | 65.74 | 1654.13 | 1235.39 | 1236.68 |
| 60 | 125.04 | 114.10 | 103.98 | 77.30 | 154.60 | 1806.41 | 1476.07 | 1490.97 |
| 59 | 200.01 | 188.92 | 133.79 | 118.72 | 237.44 | 1895.72 | 1591.32 | 1608.06 |
| 58 | 274.96 | 263.84 | 168.02 | 158.24 | 316.48 | 1818.54 | 1667.34 | 1684.51 |
| 57 | 350.01 | 338.83 | 206.17 | 199.48 | 398.95 | 2300.44 | 1698.59 | 1713.08 |





ATTENTION

VSPs in deviated wells <u>or</u> vertical wells in strongly dipping layers (>10°)

→ Strong velocity contrasts refract the P-waves and affect the std method accuracy

Improvements on standard method:

- 3C polarization method
- Ray-based tomography - FWI





Standard Walkaway VSP design



- Direct P-wave angles at receivers > ~90° (for VTI estimation)
- Reflection angles at target are < ~45° (imaging), and < ~60° (AVO)
- For imaging, the receiver array is *typically* ~1 km above the target
- For local TTI estimation, place ~12 receivers across shales of interest
- For AVO, place receivers immediately above the interfaces of interest
- In complex geology reflected points can deviate from the 2D plane and a 3D solution is required







Walkaway TTI 3D Finite Differences + RTM Imaging (Lal Khaitan et al., 2022)

→ Headwaves & multiple arrivals are properly modelled



DAS modeling – *cosine square directivity*



NOTE: recording 3DVSPs in 4 well simultaneously requires only 2 DAS boxes of latest generation





